Dr. Meyer's Marshallese subjects

402608

R

subject #	Sex	Age	Ht (cm)	Wt (kg)	TBW in L.	wt of fat kg	lean body wt kg	water (kg) total	water (kg) body wt
822	M	16	160.	54.54	38.12	~~26.45~~	~~28.09~~ 52.19	[illegible]	[illegible]
832	F	24	147.3	46.36	24.95	12.23	34.13	[illegible]	[illegible]
836	M	30	163.8	56.36	35.32	8.03	48.33	[illegible]	[illegible]
838	M	30	162.6	66.13	41.72	9.05	57.08	[illegible]	[illegible]
841	F	30	163.8	66.81	31.88	23.21	43.60	[illegible]	[illegible]
873	M	44	175.3	61.36	43.22	2.23	59.13	[illegible]	[illegible]
881	M	30	165.1	68.63	32.80	23.77	44.68	[illegible]	[illegible]
882	M	29	160.0	54.77	39.90	0.19	54.58	[illegible]	[illegible]
885	F	23	163.8	61.81	41.00	5.75	56.06	[illegible]	[illegible]
895	F	33	151.1	55.90	29.22	15.92	39.98	[illegible]	[illegible]
916	F	39	148.6	63.63	32.55	19.11	44.52	[illegible]	[illegible]
928	F	50	157.5	57.27	29.35	17.12	40.15	[illegible]	[illegible]
932	F	28	146.0	46.30	26.20	10.46	35.84	[illegible]	[illegible]
938	F	24	142.2	40.00	21.98	9.95	30.05	[illegible]	[illegible]
942	F	48	148.6	57.72	27.60	19.97	37.75	[illegible]	[illegible]
959	F	14	151.1	60.00	32.15	16.02	43.98	[illegible]	[illegible]
960	F	11	149.9	38.63	24.75	4.77	33.86	[illegible]	[illegible]
1007	M	52	163.8	71.36	41.22	14.97	56.39	[illegible]	[illegible]
1043	F	28	147.3	41.81	26.42	5.66	36.15	[illegible]	[illegible]
1501	M	30	162.6	66.81	* 43.32	* 7.54	* 59.27	[illegible]	[illegible]
Jeton	M	30	165.1	63.18	39.75	8.81	54.37	[illegible]	[illegible]

* Done by ratio method – all others done by internal standard method.

Dr. Meyer's Marshallese subjects

Subject #	Sex	Age	Ht (cm)	Wt (kg)	TBW in L.	wt of fat kg	lean body wt kg	water (kg) / Total body wt
822	M	16	160.	54.54	38.12	26.45	28.09	68.84
832	F	24	147.3	46.36	24.95	12.23	34.13	53.01
836	M	30	163.8	56.36	35.32	8.03	48.33	61.74
838	M	30	162.6	66.13	41.72	9.05	57.08	62.15
841	F	30	163.8	66.81	31.88	23.21	43.60	46.99
873	M	44	175.3	61.36	43.22	2.23	59.13	69.39
881	M	30	165.1	68.63	32.80	23.77	44.68	47.07
882	M	29	160.0	54.77	39.90	0.19	54.58	71.75
885	F	23	163.8	61.81	41.00	5.75	56.06	65.30
895	F	33	151.1	55.90	29.22	15.92	39.98	51.50
916	F	39	148.6	63.63	32.55	19.11	44.52	50.38
928	F	50	157.5	57.27	29.35	17.12	40.15	50.48
932	F	28	146.0	46.30	26.20	10.46	35.84	55.74
938	F	24	142.2	40.00	21.98	9.95	30.05	54.10
942	F	48	148.6	57.72	27.60	19.97	37.75	47.10
959	F	14	151.1	60.00	32.15	16.02	43.98	52.78
960	F	11	149.9	38.63	24.75	4.77	33.86	63.11
1007	M	52	163.8	71.36	41.22	14.97	56.39	56.90
1043	F	28	147.3	41.81	26.42	5.66	36.15	62.25
1501	M	30	162.6	66.81	* 43.32	* 7.54	* 59.27	* 42.62
Jeton	M	30	165.1	63.18	39.75	8.81	54.37	61.96

* Done by ratio method – all others done by internal standard method.

(2)

DR. L. MEYERS SUBJECTS

Subject	Sex	Age	Wt. kg	% Fat (2)	Wt. of fat in kg.	Lean body wt. (kg)	Ht cm. (in x 2.54)
822	M	16	54.54	19.36	10.56	43.98	160.0
832	F	24	46.36	19.82	9.19	37.17	147.3
836	M	30	56.36	0	0	56.36	163.8
838	M	30	66.13	6.24	4.13	62.00	162.6
841	F	30	66.81	48.82	32.31	34.50	163.8
873	M	44	61.36	0	0	61.36	175.3
881	M	30	68.63	30.39	20.86	47.77	165.1
882	M	29	54.77	— 5%	0	54.77	160.0
885	M	23	61.81	0.18	0.11	61.63	163.8
895	F	33	55.90	26.58	14.86	29.32	151.1
916	F	39	63.63	24.38	15.51	48.12	148.6
928	F	50	57.27	23.21	13.29	43.98	157.5
932	F	28	46.3	16.01	7.41	38.89	146.0
938	F	24	40.00	18.26	7.30	32.70	142.2
942	F	48	57.72	29.61	17.09	40.63	148.6
959	F	14	60.00	21.29	12.77	47.23	151.1
960	F	11	38.63	3.86	14.91	23.72	149.9
1007	M	52	71.36	19.54	13.94	57.42	163.8
1043	F	28	41.81	9.70	4.06	37.75	147.3
1501	M	30	66.81	11.29	7.54	59.27	162.6
Teton	M	30	63.18	14.21	8.98	54.20	165.1

(2)

DR. L. MEYERS SUBJECTS

Subject	Sex	Age	Wt. kg	% Fat	Wt. of fat in kg.	Lean body wt. (kg)	Ht cm. (in x 2.54)
822	M	16	54.54	19.36	10.56	43.98	160.0
832 ✓	F	24	46.36	19.82	9.19	37.17	147.3
836 ✓	M	30	56.36	0	0	56.36	163.8
838 ✓	M	30	66.13	6.24	4.13	62.00	162.6
841 ✓	F	30	66.81	48.82	32.31	34.50	163.8
873 ✓	M	44	61.36	0	0	61.36	175.3
881 ✓	M	30	68.63	30.39	20.86	47.77	165.1
882	M	29	54.77	− 5%	0	54.77	160.0
885	M	23	61.81	0.18	0.11	61.63	163.8
895	F	33	55.90	26.58	14.86	29.32	151.1
916	F	39	63.63	24.38	15.51	48.12	148.6
928	F	50	57.27	23.21	13.29	43.98	157.5
932	F	28	46.3	16.01	7.41	38.89	146.0
938	F	24	40.00	18.26	7.30	32.70	142.2
942	F	48	57.72	29.61	17.09	40.63	148.6
959	F	14	60.00	21.29	12.77	47.23	151.1
960 ✓	F	11	38.63	3.86	14.91	23.72	149.9
1007	M	52	71.36	19.54	13.94	57.42	163.8
1043 ✓	F	28	41.81	9.70	4.06	37.75	147.3
1501	M	30	66.81	11.29	7.54	59.27	162.6
Teton	M	30	63.18	14.21	8.98	54.20	165.1

Dr. Meyers subjects

6/14/63

Recount

10 Min counts

Contents	Hole #	CPM	Ratio	Efficiency	Quench Correction	CPM − Bkg	Corrected to 2 cc of 1/25 00 st
A	A	10,100	0.75	14.97	2.67	10,069	26,688
B	B	6,666	0.76	15.01	2.66	6,635	17,649
C	39	6,086	0.75	14.97	2.67	6,055	16,167
D	40	8,015	0.73	14.00	2.86	7,984	22,834
E	41	5,968	0.74	14.94	2.68	5,937	15,911
F	42	7,825	0.75	14.97	2.67	7,794	20,81c
G	43	6,508	0.74	14.94	2.68	6,477	17,358
H	44	6,134	0.75	14.97	2.67	6,103	16,29:
I	45	8,622	0.74	14.94	2.68	8,591	23,02·
J	46	7,812	0.74	14.94	2.68	7,781	20,85:
K	47	8,556	0.74	"	"	8,525	22,84,
L	48	6,555	0.74	"	"	6,524	17,484
M	49	10,078	0.74	"	"	10,047	26,92
N	50	9,638	0.75	14.97	2.67	9,607	25,65.
O	51	11,535	0.74	14.94	2.68	11,504	30,83,
P	52	9,283	0.75	14.97	2.67	9,252	24,703
Q	53	7,886	0.74	14.94	2.68	7,855	21,05,
R	54	6,106	0.73	14.00	2.86	6,075	17,374
S	55	9,997	0.75	14.97	2.67	9,966	26,609
T	56	5,937	0.73	14.00	2.86	5,906	16,891
U	57	1,958	0.76	15.01	2.66	×3.33 6,423	17,085
Bkg V	59	31	1.94	—	—		
std W1	59	10,456	0.73	14.00	2.86	10,425	29,81

1958
31
1927
3

A N
37 N
10.00 N
58,096.00 N
43,406.00 N
101,000.00 N
5,809.60
4,340.60
10,100.00
74.71

B N
38 N
10.00 N
38,131.00 N
28,877.00 N
66,664.00 N
3,813.10
2,887.70
6,666.40
75.73

C N
39 N
10.00 N
34,952.00 N
26,258.00 N
60,865.00 N
3,495.20
2,625.80
6,086.50
75.12

D N
40 N
10.00 N
46,487.00 N
34,050.00 N
80,146.00 N
4,648.70
3,405.00
8,014.60
73.24

E N
41 N
10.00 N
34,451.00 N
25,529.00 N
59,675.00 N
3,445.10
2,552.90
5,967.50
74.10

F N
42 N
10.00 N
44,926.00 N
33,760.00 N
78,254.00 N
4,492.60
3,376.00
7,825.40
75.14

G N
43 N
10.00 N
37,587.00 N
27,840.00 N
65,079.00 N
3,758.70
2,784.00
6,507.90
74.06

H N
44 N
10.00 N
35,276.00 N
26,363.00 N
61,347.00 N
3,527.60
2,636.30

74.20

H N
.44 N
10.00 N
35,276.00 N
26,363.00 N
61,347.00 N
3,527.60
2,636.30
6,134.70
74.73

I N
.45 N
10.00 N
49,697.00 N
36,961.00 N
86,223.00 N
4,969.70
3,696.10
8,622.30
74.37

J N
.46 N
10.00 N
45,173.00 N
33,363.00 N
78,116.00 N
4,517.30
3,336.30
7,811.60
73.85

K N
.47 N
10.00 N
49,547.00 N
36,488.00 N
85,563.00 N
4,954.70
3,648.80
8,556.30
73.64

L N
.48 N
10.00 N
37,808.00 N
28,099.00 N
65,550.00 N
3,780.80
2,809.90
6,555.00
74.32

M N
.49 N
10.00 N
58,085.00 N
43,238.00 N
100,785.00 N
5,808.50
4,323.80
10,078.50
74.43

N N
.50 N
10.00 N
55,495.00 N
41,409.00 N
96,379.00 N
5,549.50
4,140.90
9,637.90
74.61

O N
.51 N
10.00 N
66,574.00 N
49,410.00 N
115,351.00 N
6,657.40
4,941.00
11,535.10
74.21

P N

39,915.00 N
92,833.00 N
5,341.00
3,991.50
9,283.30
74.73
N
53 N
10.00 N
45,683.00 N
33,577.00 N
78,855.00 N
4,568.30
3,357.70
7,885.50
73.49
N
54 N
10.00 N
35,373.00 N
25,995.00 N
61,056.00 N
3,537.30
2,599.50
6,105.60
73.48
N
55 N
10.00 N
57,562.00 N
42,921.00 N
99,969.00 N
5,756.20
4,292.10
9,996.90
74.56
N
56 N
10.00 N
34,546.00 N
25,125.00 N
59,370.00 N
3,454.60
2,512.50
5,937.00
72.72
N
57 N
10.00 N
11,153.00 N
8,542.00 N
19,582.00 N
1,115.30
854.20
1,958.20
76.58
N
58 N
10.00 N
107.00 N
208.00 N
312.00 N
10.70
20.80
31.20
194.39
N
59 N
10.00 N
60,666.00 N
44,439.00 N
104,556.00 N
6,066.60
4,443.90
10,455.60
73.25

Counting water (H^3) distilled from urine by freeze drying.

Channels Ratio

832 10,363 CPM — m^{2cc} H_2O from distilled urine
— 29 Bkg
10,334 CPM Ratio 0.76 eff. 15.01

I brought all samples to the same efficiency and the unquench H3 std is 40. For sample 832 this meant multiplying CPM by 2.66 = 27,488

My std was 2 cc of distilled H_2O containing 1/25,000 of the dose the subjects took.

(All corrected to 40% counting effic.)

$$\frac{\text{Std (CPM - Bkg)}}{\text{Subject (CPM - Bkg)}} \quad \frac{29,904}{27,488} = 1.088$$

X dilution factor of 25000 = 27200
this is now Total Body Water in cc
= 27,200 L.

L x 0.985 converts to kg H_2O = 26.792 kg

$$\% H_2O = \frac{\text{Kg } H_2O}{\text{Total body wt}} = \frac{26.792}{46.36} = 57.79\%$$

$$\% \text{ Fat in Human Body} = 100 - \frac{\% H_2O}{0.72} = (80.26) = 19.74$$

wt of fat = % Fat x Bd. Wt = 9.15

Lean Body WT = Total Body wt − Fat = 46.36 kg − 9.15 kg
= 37.21 kg

int. Std. method

Subject #	Hole #	% Fat	% Fat x body wt / wt in Kg	Lean body wt (Kg)	Ht cm	wt. Kg	Sex	[illegible]
822		4.89	26.45	28.09			M	16
32		26.38	12.23	34.13			F	24
36		14.25	8.03	48.33			M	30
38		13.64	9.05	57.08			M	30
41		34.74	23.21	43.60			F	30
73		3.63	2.23	59.13			M	44
81		34.65	23.77	44.68			M	30
82		0.35	0.19	54.58			M	29
85		9.31	5.75	56.06			M	23
95		28.48	15.92	39.98			F	33
916		30.03	19.11	44.52			F	39
928		29.89	17.12	40.15			F	50
932		22.59	10.46	35.84			F	28
38		24.87	9.95	30.05			F	24
42		34.59	19.97	37.75			F	48
59		26.70	16.02	43.98			F	14
60		12.35	4.77	33.86			F	11
1007		20.98	14.97	56.39			M	52
1043		13.55	5.66	36.15			F	28
1501							M	30
Jelón		13.95	8.81	54.37			M	30

Dr. Meyer's samples done with int std 1B
the std was brought up to 2.2 cc c̄
H_2O so no water correction was made

		S 6/14/63 CPM	Vol = 2cc CPM-Bkg	Vol 2.2cc samples + int std	← 6/18/63 T-S 1.057 corrected	T-S 1.0042	(S-6) corrected for quenching	
A -	832	10,100	10 069	19 056	20,142	~~10,[illegible]~~	Ratio to 1.036	10431
B	836	6666	6635	16048	16 963	9382	1.11	7366
C	838	6086	6055	15281	16 152	10 128	1.03	6237
D	841	8015	7924	17153	18 131	10 178	1.022	8160
E	873	5968	5937	15298	16 170	10 264	1.014	6020
F	881	7825	7794	17013	17 982	10 219	1.018	7934
G.	882	6508	6477	15934	16 842	10 334	1.007	6522
H	885	6134	6103	15274	16 145	10 011	1.040	6347
I	895	8622	8591	17659	18 666	10 044	1.036	8900
J	916	7812	7781	16980	17 948	10 136	1.027	7991
K	928	8556	8525	17 565	18 566	10 010	1.040	8866
L	822	6555	6524	15 618	16 508	9953	1.046	6824
M	960	10,078	10,047	18951	20 031	9 953	1.046	10,50[illegible]
N	932	9638	9607	18640	19 702	10 064	1.034	9934
O	938	11535	11,504	20 481	21 648	10113	1.029	11838
P	942	9283	9252	18446	19 497	10214	1.019	9428
Q	959	7886	7855	17024	17 994	10 108	1.030	8091
R	1007	6106	6075	15250	16 119	10013	1.039	6310
S	1043	9997	9966	19429	20 536	10 539	0.988	9846
T	1501	5937	5906	~~12548~~	~~13 263~~	~~7 326~~	~~1.421~~	
U	Jeton	1958 (X3.33	6417	11 504	12,160	10,202	1.020	6545
V	Bkg	31	31	28	—			
W*	std	10,456	10,425 ☆	9,847	$\boxed{10,408}$	—		
~~Z~~	std	2cc of 1/25000 std		10,351				
W	std			10,440				

* same ppt as used to prepare patient dose
☆ brought up to 2.2cc H_2O c̄ dist H_2O

(2) Dr. Meyer's patients Int Std method

Subject #	Ratio std cts-Bkg / subject cts-Bkg	Ratio x 2.5x10^4	TBW in L	L x 0.985 L converted to Kg	% H_2O Kg H_2O / Kg Body wt	col. 1 % Fat 100 - % H_2O / 0.72
822	1.525	38,125	38.12 L	37.55	68.84	100 - 95.11
32	0.998	24,950		24.58	53.01	73.65
36	1.413	35,325		34.80	61.74	85.75
38	1.669	41,725		41.10	62.15	86.31
41	1.275	31,875		31.40	46.99	65.2
73	1.729	43,225		42.58	69.39	96.37
81	1.312	32,800		32.31	47.07	65.3
82	1.516	39,400		39.30	71.75	99.6
85	1.640	41,000		40.38	65.30	90.6
85	1.169	29,225		28.79	51.50	71.5
916	1.302	32,550		32.06	50.38	69.9
28	1.174	29,350		28.91	50.48	70.1
32	1.048	26,200		25.81	55.74	77.4
38	0.879	21 975		21.64	54.10	75.2
42	1.104	27600		27.19	47.10	65.4
59	1.286	32150		31.67	52.78	73.3
60	0.990	24 750		24.38	63.11	87.65
1007	1.649	41 225		40.607	56.90	79.0
1043	1.057	26 425		26.03	62.25	86.4
1501						
Jetton	1.590	39 750		39.15	61.96	86.0

(1)

Dr Meyer's subjects

5/27/63

(1)

Bott	Bottle #	Machine Hole #	CPM		Ratio	efficiency ~~Quench correction~~	Quench correction	corrected to 2cc 1/25,000 std corrected counts
832	A	21	10,363	10,334	0.76	15.01%	2.66	27,488
836	B	22	6,746	6717	0.76	15.01	2.66	17,867
838	C	23	6,227	6198	0.76	15.01	2.66	16,487
841	D	24	8,187	8158	0.75	14.97	2.67	21,782
873	E	25	6,170	6141	0.75	14.97	2.67	16,396
881	F	26	8,044	8015	0.75	14.97	2.67	21,400
882	G	27	6,681	6652	0.76	15.01	2.66	17,694
885	H	28	6,213	[illegible]	0.74	14.94	2.67	16,573
895	I	29	8,738	[illegible]	0.73	14.[illegible]	2.[illegible]	24,908
916	J	30	8,019	[illegible]	0.76	15.01	2.66	21,248
928	K	31	8,737	8708	0.75	14.97	2.67	23,250
822	L	32	6,801	6772	0.75	[illegible]	2.67	18,081
960	M	33	10,336	10,307	0.75	[illegible]	2.67	27,520
932	N	34	9,875	9846	0.74	14.[illegible]	2.67	26,289
938	O	35	11,742	11,713	0.74	[illegible]	2.67	[illegible]
942	P	36	9,490	9461	0.76	15.01	2.66	25,166
959	Q	37	8,136	8107	0.75	14.97	2.67	21,646
1007	R	38	6,253	6224	0.73	14.00	2.86	17,801
1043	S	39	10,128	[illegible]	0.74	14.94	2.68	27,066
1501	T	40	6,060	[illegible]	0.73	14.00	2.86	17,249
JETON	U	41	1,942 x3.33=6370	1913	0.72	13.50	[illegible]	18,855
BKG	V	42	29	—	2.22			
Std 1/25,000	W	43	10,540	10,511	0.76	15.01	2.66	27,959
1/25,000 *	W'	109	10,485	10,456	0.73	14.00%	2.86	29,904

* Jeton only 0.6cc distilled H_2O from urine — so I added 1.4 cc distilled H_2O to equate all quenchings — The CPM of 0.6cc HTO should be multiplied by 3.33 to bring it in line

DR MEYER'S CASES

5/27/63

RATIO

Case #	Bottle #	Hole #	CPM	CPM − BKg	RATIO	Eff	Quench correction Ratio (to bring all up to 40%)	CPM − BKg × QCF
822	L	32	6801	6772	.75	14.97	2.67	18081
32	A	21	10363	10,334	.76	15.01	2.66	27488
36	B	22	6746	6717	.76	15.01	2.66	17867
38	C	23	6227	6198	.76	15.01	2.66	16487
41	D	24	8187	8158	.75	14.97	2.67	21782
73	E	25	6170	6141	.75	14.97	2.67	16396
81	F	26	8044	8015	.75	14.97	2.67	21400
82	G	27	6681	6652	.76	15.01	2.66	17694
85	H	28	6213	6184	.74	14.94	2.68	16573
95	I	29	8738	8709	.73	14.00	2.86	24908
916	J	30	8017	7988	.76	15.01	2.66	21248
28	K	31	8737	8708	.75	14.97	2.67	23250
32	N	34	9875	9846	.74	14.94	2.68	26289
38	O	35	11742	11713	.74	14.94	2.68	31274
42	P	36	9490	9461	.76	15.01	2.66	25166
59	Q	37	8136	8107	.75	14.97	2.67	21646
60	M	33	10336	10307	.75	14.97	2.67	27520
1007	R	38	6253	6224	.73	14.00	2.86	17801
1043	S	39	10128	10,099	.74	14.94	2.68	27066
1501	T	40	6060	6031	.73	14.00	2.86	17249
Jeton	U	41	1942 + 1333 = 6370	1913 − 6370	.72	13.50	2.96	18855
BKg	V	42	29	—	2.22			
Std *	W'	109	10,485	10456	.73	14.00	2.86	29904
Std	W	43	10540	10511	.76	15.01	2.66	27959

(2) DR. L. MEYERS SUBJECTS

Subject	Sex	Age	Wt. Kg	% Fat (2)	Wt. of fat in Kg.	Lean body wt (Kg)	Ht in x 2.54 cm
822	M	16	54.54	~~19.36~~ 0	0	43.98	160.0
832	F	24	46.36	19.82	9.19	37.17	147.3
836	M	30	56.36	0	0	56.36	163.8
838	M	30	66.13	6.24	4.13	62.00	162.6
841	F	30	66.81	48.82	32.31	34.50	163.8
873	M	44	61.36	0	0	61.36	175.3
881	M	30	68.63	30.39	20.86	47.77	165.1
882	M	29	54.77	— 5%	0	54.77	160.0
885	M	23	61.81	0.18	0.11	61.63	163.8
895	F	33	55.90	26.58	14.86	29.32	151.1
916	F	39	63.63	24.38	15.51	48.12	148.6
928	F	50	57.27	23.21	13.29	43.98	157.5
932	F	28	46.3	16.01	7.41	38.89	146.0
938	F	24	40.00	18.26	7.30	32.70	142.2
942	F	48	57.72	29.61	17.09	40.63	148.6
959	F	14	60.00	21.29	12.77	47.23	151.1
960	F	11	38.63	3.86	14.91	23.72	149.9
1007	M	52	71.36	19.54	13.94	57.42	163.8
1043	F	28	41.81	9.70	4.06	37.75	147.3
1501	M	30	66.81	11.29	7.54	59.27	162.6
Jeton	M	30	63.18	14.21	8.98	54.20	165.1

(3)

Subject #	Ratio Std / Subject, 1.654	R×25000	TBW in L	L×0.985 Liters converted to kg	% H_2O Kg H_2O / Kg bodywt	% Fat (1) 100 − % H_2O / 0.72
		41,350	41.350			
		~~32,150~~	~~32.150~~	40.730	74.48 ~~38.06~~	103%
828	~~1.806~~	~~27,175~~	~~27.175~~	~~31.668~~	~~34.00~~	~~80.64~~
832	1.087	27,175	27.175	26.767	57.73	80.18
836	1.673	41,825		41.198	73.09	101.51
838	1.813	45,325		44.645	67.51	93.76
841	1.372	25,000		24.625	36.85	51.18
873	1.823	45,575		44.891	73.16	101.61
881	1.397	34,925		34.401	50.12	69.61
882	1.690	42,250		41.616	75.98	105.53
885	1.804	45,100		44.424	71.87	99.82
895	1.200	30000		29.550	52.86	73.42
916	1.407	35175		34.647	54.45	75.62
928	1.286	32150		31.668	55.29	76.79
932	1.137	28425		27.999	60.47	83.99
938	0.956	23900		23.542	58.85	81.74
942	1.188	29700		29.255	50.68	70.39
959	1.381	34525		34.007	56.67	78.71
9600	1.086	27150		26.743	69.22	96.14
1007	1.679	41975		41.345	57.93	80.46
~~1043~~	1.104	27600	27.186		65.02	90.30
1501	1.733	43325		42.675	63.87	88.71
Jeton	1.585	39625		39.031	61.77	~~85.79~~

~~Method~~

#832 S 10,100 CPM in 2cc distilled H_2O
− 31 BKg
(S-b) 10,069 CPM
+ int std (200λ) − of $\frac{1}{25}$ CC dose
T 19,056 CPM → this is corrected back to 2cc since the 200λ std have caused some quenching

T = 20,142
T-S = − 10,042 ← this activity is from the int std
The std is 2cc ~~H2O~~ int std + 200λ ~~int std~~ H_2O
the counts are corrected back to 2cc −
Std 10,408 CPM (all due to int std)

correction for quenching

$$\frac{\text{std T}}{\text{subject T}} \quad \frac{10,408}{10042} = 1.036.$$

$$(S-b) \times 1.036 = 10,431 \text{ CPM}$$

$$\frac{\text{Std cts}}{\text{Subject counts}} = \frac{10408}{10431} = 0.998 \times \text{dilution factor of std.}$$

$0.998 \times 25000 = 24950$ cc = Total Body Water
Convert to Kg H_2O = 24.95 Kg
% H_2O = $\frac{24.95}{46.36}$ = 53.02

% Fat = $100 - \frac{\% H_2O}{0.72} = 100 - 73.64 = 26.36$ %

Kg of Fat = 12.22 kg